

## Magnetic Composite for Efficient Adsorption of Iron and Manganese Ions from Aqueous Solution

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### ABSTRACT

Iron Fe(III) and Manganese Mn(II) ions were effectively removed from aqueous solutions using a magnetic composite of Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA, with CaO sourced from green mussel. The composite material was comprehensively characterized using Fourier Transform Infrared Spectroscopy (FTIR), X-ray Diffraction (XRD), Scanning Electron Microscopy with Energy Dispersive – X-ray Spectroscopy (SEM-EDS), Brunauer, Emmett and Teller (BET) surface area analysis, Vibrating Sample Magnetometer (VSM). The impact of physicochemical adsorption parameters, such as solution pH, contact time, and concentration, were investigated. The Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composite displayed a value of 51.47 emu/g in saturation magnetization, enabling rapid separation through the use of an external magnet without the need for filtration. Optimal conditions for adsorbing Fe(III) ions were achieved at pH 3 and initial concentration of 400 mg/L with maximum efficiency reach after 60 minutes. Similarly, optimal conditions for Mn(II) ion adsorption were observed at pH 4 with the same contact time and initial concentration. The adsorption efficiencies were found to be 88.56% for Fe(III) and 75.65% for Mn(II). The pseudo-second-order model aptly depicted the kinetics associated with the adsorption of both types of ions while the Langmuir isotherm model indicated that monolayer adsorption takes place on the composite's surface. The maximum capacities for adsorption is 322.58 mg/g for Fe(III) ions and 208.33 mg/g for Mn(II) ions. A negative Gibbs free energy value affirmed that the process occurs spontaneously under natural conditions. These results underscored the potential use of this Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composite in treating wastewater to remove heavy metal ions.

**Keywords:** magnetic composite; adsorption; iron and manganese ions

### INTRODUCTION

Currently, the environmental repercussions of mining are a significant global concern (Valente et al., 2015; Nunex-Gomez et al., 2019). The extraction and processing of coal result in the disposal of wastewater in open areas that are particularly rich in pyrite. The oxidation process occurs in the presence of water, oxygen, and microbes, forming Acid Mine Drainage (AMD) (Mokgehle and Tawengwa, 2021; Kobielska et al., 2018). In addition, it should be noted that AMD possesses the ability to dissolve heavy metal ions.

Consequently, the defining attributes of AMD include a low pH level, typically below 4.0, as well as elevated concentrations of sulfides and various heavy metal including but not limited to Fe, Al, Mn, Cu, Zn, Pb, Ni, Cd, and Co (Nunex-Gomez et al., 2019; Yang et al., 2021). AMD presents a considerable risk of contaminating both underground and surface water bodies, thereby creating substantial environmental issues that can negatively affect ecosystems and human health (Ren et al., 2022; Favere et al., 2004). Metal ions with high atomic weights pose challenges for natural decomposition processes, as they have a tendency

to infiltrate the food chain and accumulate within animals (Masindi et al., 2015).

The concentrations of heavy metals in AMD have been lowered using a variety of different approaches. These methods include sulfidogenic bioreactors (Deng et al., 2016), reverse osmosis (Ambiado et al., 2017), membrane filtration (Menzel et al., 2021), electrocoagulation using  $\text{Ca}(\text{OH})_2$  (Stylianou et al., 2022), microalgae phycoremediation (Chen et al., 2023), and adsorption using layered double hydroxides (Xu et al., 2023). There is an immediate need for AMD processing technologies that are not only effective but also affordable and capable of eliminating significant quantities of metal ions. There is reason to be optimistic about the adsorption approach to solving this issue.

CaO, a potential natural adsorbent for the removal of heavy metal ions, can be sourced from a diverse range of materials. For instance, cow bones (Ayodeji, 2018), eggshells (Hossain et al., 2021), cockle shells (Mohamed et al., 2016), fish bones (Mostofa et al., 2022), and mollusk shells (Thakur et al., 2021) have all been identified as viable sources. Additionally, mussel shells – a type of shellfish widely consumed in Indonesia – are also an abundant source of CaO (Purwaningrum et al., 2022). Approximately 20% of the shellfish constitute the edible portion, while the remaining 75–90% comprises the shell. The composition of the mussel shell is mainly consisting of approximately 95% CaO, with the remaining constituents comprising organic matter and various other components (Aguila-Almanza et al., 2022; Hamestera et al., 2012). Hence, it is imperative to undertake the processing of mussel shell in order to mitigate environmental pollution.

The production of CaO can be achieved by subjecting  $\text{CaCO}_3$  to elevated temperatures (Hossain et al., 2023). The utilization of natural adsorbents has been found to result in reduced operational expenses and exhibit environmentally sustainable characteristics. It is essential to acknowledge that natural adsorbents possess certain limitations, most notably their relatively low adsorption capacity. Hence, it is imperative to devise a novel adsorbent that can effectively address these constraints, primarily by modifying the adsorbent material. The formation of  $\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$  composite can be achieved by modifying CaO with  $\text{Fe}_3\text{O}_4$  and polydopamine (PDA) compounds. Incorporating a superparamagnetic core, like  $\text{Fe}_3\text{O}_4$ , during the post-adsorption phase significantly improves efficiency. It allows for quick

adsorbent separation from the solution using a permanent magnet. This method is more economical than traditional filtration and centrifugation techniques (Hariani et al., 2021).

PDA is recognized for its biocompatibility and its unique ability to form a consistent layer that is hydrophilic in nature. This layer, characterized by functional groups on its surface, originates from the self-polymerization process of dopamine under alkaline buffer conditions. With superior adhesive characteristics and beneficial reducibility, PDA plays a crucial role in preventing  $\text{Fe}_3\text{O}_4/\text{CaO}$  from clustering (Yang et al., 2019). The versatility of PDA as an adsorbent has been showcased in various studies. For example,  $\text{Fe}_3\text{O}_4/\text{PDA}/\text{PANI}$  has been utilized as an adsorbent for eliminating tartrazine and Sunset yellow (Miri et al., 2021),  $\text{MnO}_2/\text{PDA}/\text{Fe}_3\text{O}_4$  demonstrated potential for Pb(II) ions adsorption (Shi et al., 2021), and  $\text{AMP}/\text{PDA}/\text{Fe}_3\text{O}_4$  proved effective for Cs(I) and U(VI) adsorption (Li et al., 2023).

This research aims to fabricate a  $\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$  composite using CaO sourced from green mussel shells. The characterization of this composite will involve methods such as FTIR, SEM-EDS, BET surface area analysis, XRD, and VSM. The main application of the synthesized composite will be for the adsorption of heavy metal, with a particular focus on Fe(III) and Mn(II) ions.

## MATERIALS AND METHODS

### Materials

The current investigation utilized a range of chemicals including but not limited to Iron(III) chloride hexahydrate, ethanol, Iron(II) chloride tetrahydrate, hydrochloric acid and sodium hydroxide. Additionally, Tris-Hydrochloride (Tris-Cl), Dopamine (DA), and standard solutions of Iron(II), Iron(III), and manganese(II) each with a concentration of 1000 ppm were used. All these chemicals were procured from Merck in Germany. Green mussel shells also played a part in the research process.

### CaO preparation

The production of CaO in this study adheres to the method detailed by Purwaningrum et al. (2022). The process begins with the cleaning of green mussel shells to rid them of impurities. This is achieved by first rinsing the shells with distilled

water and subsequently boiling them for half an hour. Post-cleaning, the shells are oven-dried at a temperature of 100°C for a duration of two hours. Following this, the material is subjected to ball milling to obtain finer particles. The milled product is then calcinated in a muffle furnace at 800°C for an hour, with the temperature increasing at a steady rate of 3.5°C per minute. Finally, CaO is preserved in separate air-tight polyethylene bags to maintain its quality and prevent exposure to air.

### The synthesis of Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composite

The synthesis of the Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composite was a two-step process. Initially, a Fe<sub>3</sub>O<sub>4</sub>/CaO composite was synthesized, adhering to a Fe<sub>3</sub>O<sub>4</sub> to CaO mass ratio of 1:2. In total, 4.66 g of FeCl<sub>2</sub>·6H<sub>2</sub>O and 1.72 g of FeCl<sub>2</sub>·4H<sub>2</sub>O were collectively dissolved into a volume of 25 mL distilled water. This solution was mechanically stirred, while being continuously purged with nitrogen gas and heated to 60°C, followed by the gradual addition of 4 g CaO. Thereafter, a 1 M NaOH solution was introduced gradually until the solution reached a pH of 10. The resulting solid substance underwent washing with distilled water and ethanol until it attained neutral pH, after which it was dried in an oven at a temperature setting of 80°C for one hour. The second stage of the synthesis involved combining 2.0 g of CaO/FeO, 0.133 g of DA, and 0.22 g of Tris-Cl in a fresh volume (30 mL) of distilled water to create the final Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composite. The solution was then sonicated for two hours at room temperature, after which any suspended particles were separated via centrifugation at a speed of 3500 rpm for 30 minutes. The product was repeatedly washed with distilled water until it reached a neutral pH level. The solid material was then extracted from the solution using an external magnet and subsequently dried in an oven set at 105°C for two hours.

## CHARACTERIZATION

The analysis of the phase and crystal structure was executed using XRD (XRD PANalytical), with the settings being a 50-mA current, a 40 kV voltage, and CuK $\alpha$  radiation of 1.546 Å wavelength. BET technique was used to assess the surface area and pore size distribution of the adsorbent, involving nitrogen adsorption-desorption cycles on a QuadraSorb station 1 7.01. The

morphology and elemental composition were examined using SEM-EDS (JOEL JSM 6510 LA). The magnetic characteristics of the adsorbent were probed using a VSM of Oxford Type 1.2 T model. FTIR conducted on a Prestige-21 Shimadzu instrument in the spectral range between 400–4000 cm<sup>-1</sup>, was used for functional group analysis. Lastly, AAS on a Shimadzu AA 7000 was used to determine metal ion concentrations.

## Adsorption

The adsorption capacity of the Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composite for Fe(III) and Mn(II) ions was assessed in this study. Various parameters were considered, including pH, contact time, initial concentration of metal ions in the solution, and temperature. The pH levels were adjusted to fall within a range of 1.5 to 5 using either a 1 M HCl or NaOH solution. The contact duration was varied between 0 and 70 minutes, while the initial concentration of ions in the solution was set within a range from 100 to 450 mg/L. Adsorption kinetics were examined by observing changes over varying contact times, while adsorption isotherms were derived from studying variations in the initial concentrations of metal ions. Thermodynamic parameters were evaluated by tracking temperature changes at specific points: specifically at 25°C, 35°C, 45°C, and 55°C. Finally, a mathematical equation was used to calculate the adsorption capacity based on these experimental conditions.

$$q_e = \frac{V(C_0 - C_t)}{m} \quad (1)$$

where:  $C_0$  represent the initial, while and  $C_t$  final concentrations of metal ions (mg/L), respectively.

$V$  stands for the solution's volume (L), while  $m$  indicates the adsorbent mass (g).

## RESULTS AND DISCUSSION

### Characterization of Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composite

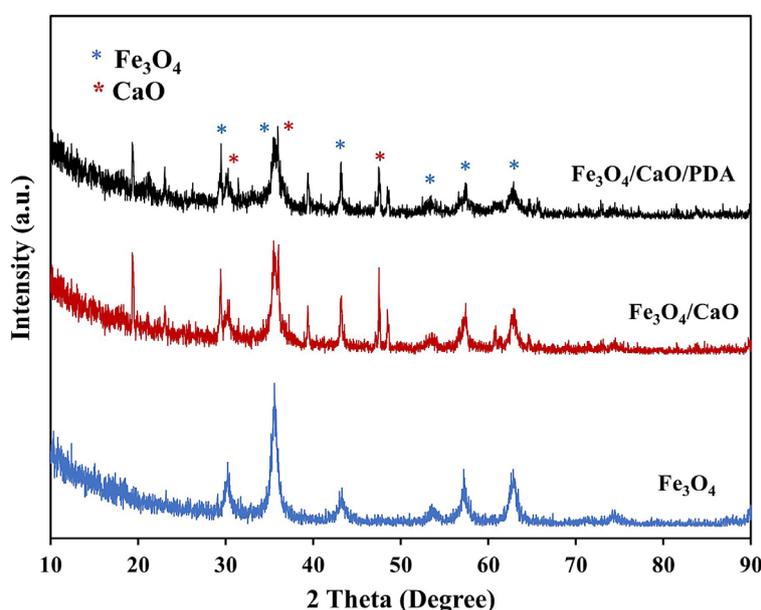
Figure 1 presents the XRD spectra of Fe<sub>3</sub>O<sub>4</sub>, Fe<sub>3</sub>O<sub>4</sub>/CaO, and Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA. The distinctive peaks of Fe<sub>3</sub>O<sub>4</sub> are seen at angles 30.4°, 35.47°, 43.35°, 53.71°, 57.27°, and 62.63°, which are

associated with the crystal planes [220], [311], [400], [422], [511], and [440] in that order as confirmed by JCPDS card No. 19–0629.  $\text{Fe}_3\text{O}_4/\text{CaO}$  composite peaks exhibit a reduction in intensity, with some overlap observed between the  $\text{Fe}_3\text{O}_4$  peak and the appearance of new peaks originating from CaO. These new peaks, specifically at  $32.09^\circ$ ,  $36.10^\circ$ , and  $46.54^\circ$  (JCPDS card No. 48–167), can be attributed to CaO. No discernible difference was observed in the diffraction peak of the  $\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$  composite compared to that of the  $\text{Fe}_3\text{O}_4/\text{CaO}$  composite. However, the peak intensity of the  $\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$  composite was lower than that of the  $\text{Fe}_3\text{O}_4/\text{CaO}$  composite. It suggests that PDA lacks a definite form or structure (Shi et al., 2021).

An adsorbent's ability to adsorb is heavily dependent on its surface area. Table 1 provides the measurements of surface areas for CaO,  $\text{Fe}_3\text{O}_4/\text{CaO}$ , and  $\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$  composites. As per Buasri et al. (2013), the derived surface area ( $86.554 \text{ m}^2/\text{g}$ ) surpasses that of CaO obtained from cooke shell ( $59.87 \text{ m}^2/\text{g}$ ) and scallop shell ( $74.96 \text{ m}^2/\text{g}$ ).  $\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$  composites demonstrated a relatively diminished surface area in

comparison to  $\text{Fe}_3\text{O}_4/\text{CaO}$ , implying the integration of both  $\text{Fe}_3\text{O}_4$  and PDA elements within the composite structure. It has been observed that  $\text{Fe}_3\text{O}_4$  tends to occupy the pores within CaO. A similar phenomenon was also reported in previous research where inclusion of  $\text{Fe}_3\text{O}_4/\text{PDA}$  in the  $\text{Fe}_3\text{O}_4/\text{PDA}/\text{HKUST-1}$  composite led to a reduction in surface area (Zhou et al., 2023). These observations suggest that incorporation of both  $\text{Fe}_3\text{O}_4$  and PDA resulted in an expansion in pore diameter when using Barrett-Joyner-Halenda (BJH) adsorption methodology; however, there was a decrease in pore volume. These pores are categorized as mesopores with diameters ranging from 2 to  $50 \text{ \AA}$  (Duan et al., 2020).

Figure 2 illustrates the morphological of CaO,  $\text{Fe}_3\text{O}_4/\text{CaO}$ , and  $\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$  composites. The surface of CaO exhibited an uneven structure. However, notable changes were seen upon introducing  $\text{Fe}_3\text{O}_4$  and subsequent coating with PDA. Specifically, the surface became rougher, displaying a plate-like morphology, and the emergence of white PDA particles on the surface was evident. The outcomes corroborate the depiction in Figure 3, demonstrating a heterogeneous elemental

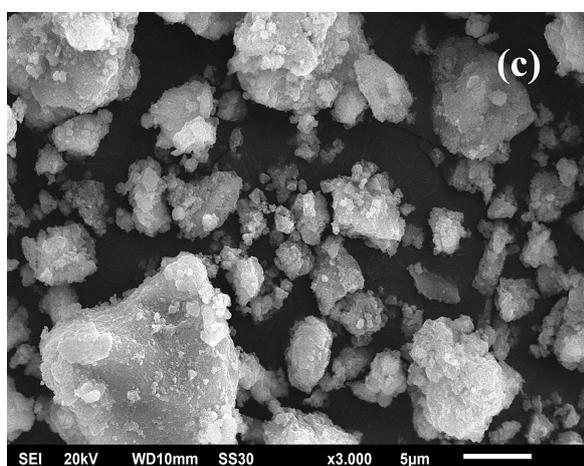
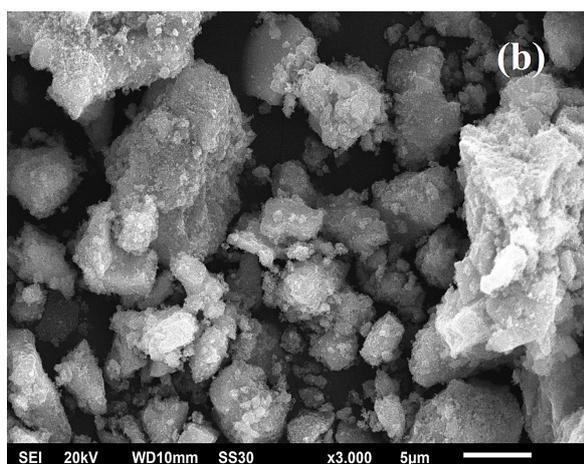
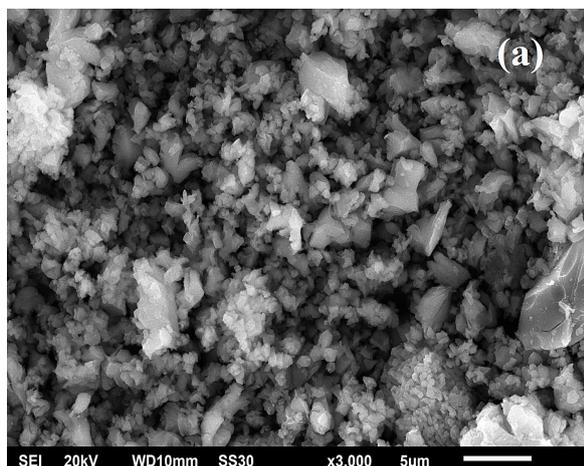


**Figure 1.** XRD spectra of  $\text{Fe}_3\text{O}_4$ ,  $\text{Fe}_3\text{O}_4/\text{CaO}$  and  $\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$  composites

**Table 1.** The result of surface area measurement of CaO,  $\text{Fe}_3\text{O}_4/\text{CaO}$  and  $\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$  composites

Adsorbent	BET surface area ( $\text{m}^2/\text{g}$ )	Pore volume ( $\text{cm}^3/\text{g}$ )	Pore diameter ( $\text{\AA}$ )
CaO	86.554	0.171	15.14
$\text{Fe}_3\text{O}_4/\text{CaO}$	74.840	0.161	16.89
$\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$	64.302	0.113	20.41

dispersion across the surface of the  $\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$  composite. A significant presence of Fe (represented by blue color) implies that  $\text{Fe}_3\text{O}_4$  not only fills up the pores of CaO but also adheres to its surface. The results from the EDS analysis indicated that the composition of CaO was made up of 68.06% Ca and 31.94% O. The successful



**Figure 2.** Morphology of (a) CaO, (b)  $\text{Fe}_3\text{O}_4/\text{CaO}$ , and (c)  $\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$  composites

synthesis of the  $\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$  composite is corroborated by the detection of Ca, O, Fe, C, and N elements as demonstrated in Table 2.

Figure 4 illustrates the correlation between magnetization and the magnetic field. The  $\text{Fe}_3\text{O}_4/\text{CaO}$  composite demonstrated superior magnetic properties in comparison to the  $\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$  composite, as indicated by their respective values of 66.28 emu/g and 51.47 emu/g. The reduction in magnetic properties can be ascribed to the non-magnetic PDA coating. As per Shi et al. (2021) findings,  $\text{PDA}/\text{Fe}_3\text{O}_4$  exhibits a saturation magnetization of 37 emu/g, which is higher than that of  $\text{MnO}_2/\text{PDA}/\text{Fe}_3\text{O}_4$ . The use of these magnetic characteristics provides numerous advantages in terms of efficiency and cost-effectiveness due to the capability for straightforward separation of the adsorbent from the solution using an external magnet, thereby facilitating rapid separation (Hariyani et al., 2021).

#### Batch adsorption of Fe(III) and Mn(II) ions

The pH level exerts a pivotal influence on the adsorption process. This investigation scrutinized the impact of pH, spanning from 1.5 to 5, on the adsorption of Fe(III) and Mn(II) ions, which were employed at concentrations of 100 mg/L and 50 mg/L. The dosage of the composite was fixed at 0.1 g/L, while the stirring speed was kept constant at 150 revolutions per minute. The correlation between initial pH and intrinsic structural attributes of both the adsorbent substance and metal ions has been previously elucidated by Shi et al. (2021).

As illustrated in Figure 5(a), there is a direct correlation between pH level and the amount of metal ions adsorbed. At lower pH values, competition arises between positively charged metal ions and  $\text{H}^+$  ions for interaction with PDA, which contains O and OH groups (Mansoor & Abbasitabar, 2020; Yang et al., 2021). The optimal pH to achieve maximum adsorption capacity was found to be at a value of 3 for Fe(III) ions and at a value of 4 for Mn(II) ions. Beyond these optimal points, any further increase in pH does not enhance adsorption capacity due to formation of  $\text{Fe}(\text{OH})_3$  and  $\text{Mn}(\text{OH})_2$ .

This behavior mirrors trends observed in other studies such as that conducted by Brishti et al. (2023), where activated carbon derived from Bombax ceiba fruit shell was used for adsorption of Fe(III) ions with peak efficiency reached at a pH value of around 3.5 before plateauing until about

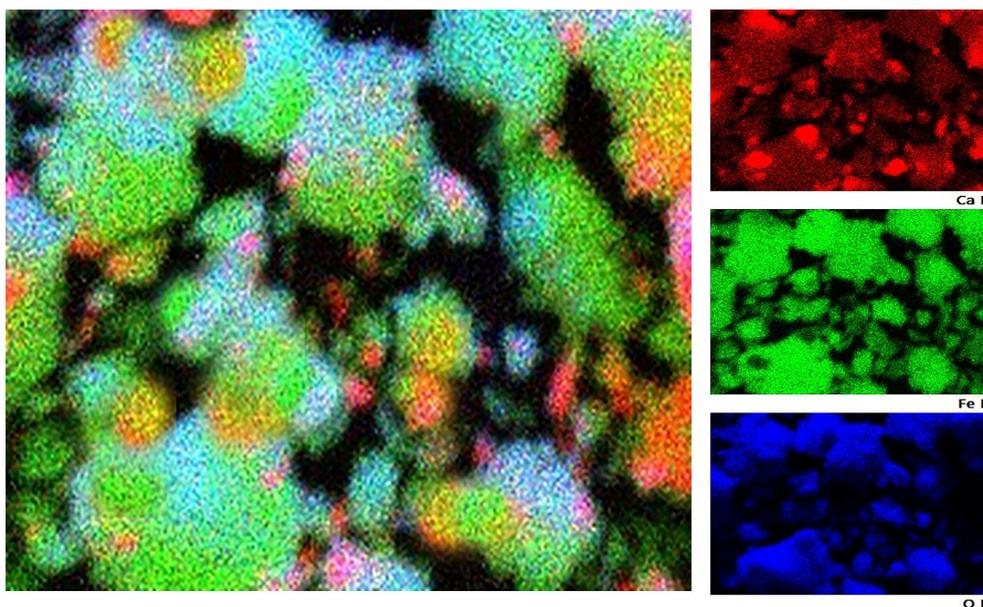


Figure 3. SEM mapping of Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composite

Table 2. Elemental composition of CaO, Fe<sub>3</sub>O<sub>4</sub>/CaO, and Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composites from EDS analysis

Content, %	CaO	Fe <sub>3</sub> O <sub>4</sub> /CaO	Fe <sub>3</sub> O <sub>4</sub> /CaO/PDA
Ca	68.06	26.27	15.32
O	31.94	41.69	34.10
Fe	-	32.04	19.07
C	-	-	29.23
N	-	-	2.28

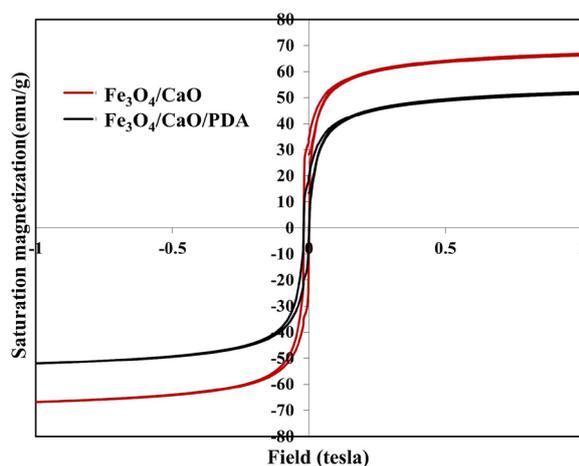


Figure 4. Hysteresis loops of Fe<sub>3</sub>O<sub>4</sub>/CaO and Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composites

pH value of approximately 5.5. Similarly, another study involving Mn ion absorption using activated carbon derived from banana peel showed optimal performance occurring at a similar point – specifically when reaching a slightly higher pH value around about 4 (Khairiah et al., 2021).

The contact time was optimized over a range of 5 to 60 minutes. The concentration of Fe(III) ions was set at 100 mg/L, and Mn(II) ions were kept at 50 mg/L. A composite dosage of 0.1 g/L was utilized, and the pH of the solution was adjusted to 3 for Fe(III) ions and to 4 for Mn(II) ions. The agitation speed was maintained at 150 rpm. As shown in Figure 5(b), there is an initial rapid uptake of metal ions, which subsequently slows down as it approaches equilibrium—this observation is consistent with prior research by El Shawayy et al. (2022) and Brishti et al. (2023). At a contact time of just five minutes, the adsorption capacity for Fe(III) ions reached 51.23 mg/g, whereas it measured at 17.67 mg/g for Mn(II) ions. After a full hour (60 minutes), these capacities increased to 88.56 mg/g for Fe(III) ions and to 37.93 mg/g for Mn(II) ions respectively.

Figure 5(c) presents data that indicates a direct relationship between the rate of adsorption and the initial concentration of metal ions. The study conducted this adsorption process across a concentration range of 100–450 mg/L.

The upward trend can be ascribed to remaining pores or active sites on the adsorbent material that maintain their capability to attach to metal ions. However, once these sites reach saturation, they lose their ability to accommodate additional metal ions (Brishti et al., 2023). No noticeable increase in metal ion adsorption was observed for both Fe(III) and Mn(II) ions at an initial concentration of 450 mg/L.

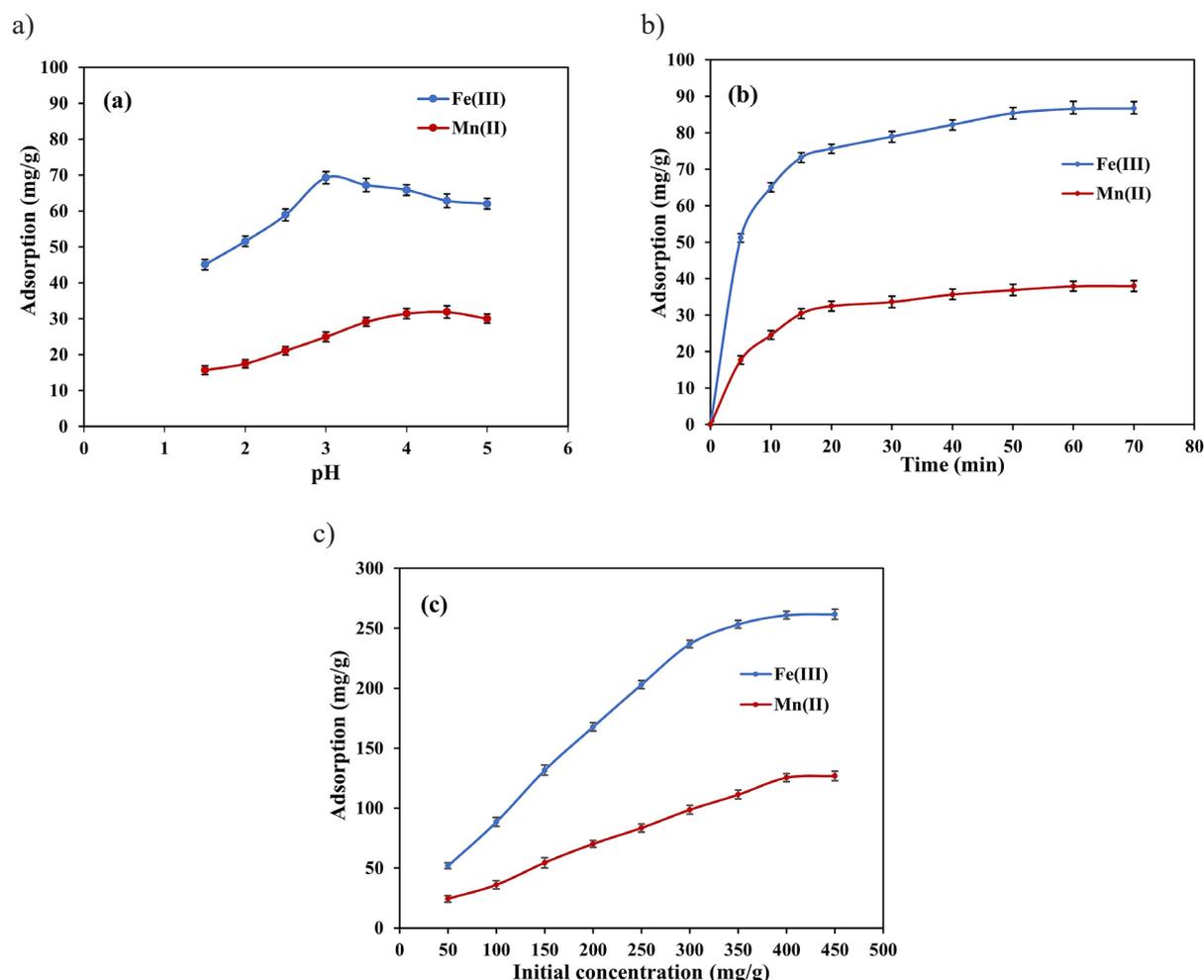
### FTIR spectra of composite pre- and post-adsorption

Figure 6 presents the spectra of the  $\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$  composite before and after the adsorption procedure. The spectra reveal a broad peak within the  $3200\text{--}3400\text{ cm}^{-1}$  range, indicative of O–H and N–H stretching vibrations. A band at  $1600\text{ cm}^{-1}$  corresponds to N–H bond movements, encompassing both stretching and bending modes (Touqeer et al., 2020). A peak located at  $1290\text{ cm}^{-1}$  suggests the existence of a C–O bond.

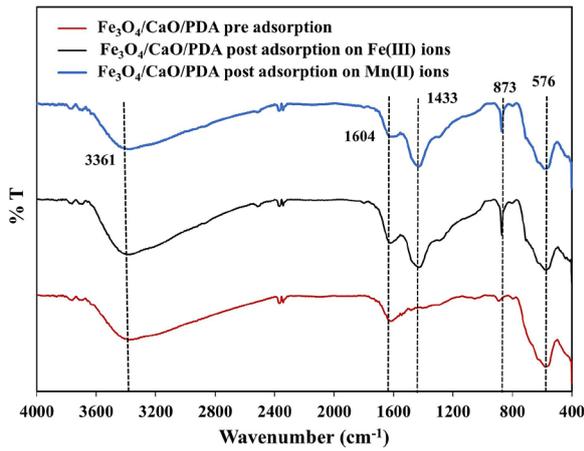
All three spectra feature an Fe–O band located at  $569\text{ cm}^{-1}$ , indicative of  $\text{Fe}_3\text{O}_4$ 's presence. According to Legodi et al. (2001), a peak appearing between  $1400\text{--}1500\text{ cm}^{-1}$  together with another near  $873\text{ cm}^{-1}$  implies swift transformation from hydroxide into carbonate. This specific peak can be seen in the spectra for the  $\text{Fe}_3\text{O}_4/\text{CaO}/\text{PDA}$  composite following the ions adsorption. As delineated by Kasirajan et al. (2022), any shift in wavenumber below  $10\text{ cm}^{-1}$ , accompanied by alterations in peak intensity, is indicative of the formation of metal ion bonds with the adsorbent substrate.

### Adsorption kinetics and isotherm

The importance of kinetics in evaluating the effectiveness of adsorption is underscored in the work of Moghadam et al. (2013). Within the realm of adsorption kinetics, two models are predominantly used: the pseudo-first-order and pseudo-second-order models. These can be signified mathematically through these equations.



**Figure 5.** The impact of variable on the adsorption including (a) pH, (b) Contact time, and (c) Initial concentration.



**Figure 6.** The comparison of FTIR spectra of the Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composite pre- and post-adsorption.

$$\ln(q_e - q_t) = \ln q_e - k_1 t \quad (2)$$

$$\frac{t}{q_t} = \frac{1}{k_2 q_e^2} + \frac{t}{q_e} \quad (3)$$

The variables  $q_t$  (mg/g) are indicative of the adsorption potential at a given time ( $t$ ), while  $q_e$  (mg/g) denotes the potential when equilibrium is reached. The parameters  $k_1$  (min<sup>-1</sup>) correspond to the equilibrium states of pseudo-first-order, whereas  $k_2$  (g/mg.min) pseudo-second-order reactions. The pseudo-second-order model exhibits a superior regression coefficient ( $R^2$ ) when compared to the first-order model, suggesting that it provides a more accurate representation of the adsorption dynamics of Fe(III) and Mn(II) ions onto the Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composite.

The pseudo-first-order process characterizes a reversible reaction that creates an equilibrium between the solid and liquid phases. In contrast, the pseudo-second-order process implies chemical adsorption takes place (Yang et al., 2021). The adsorption capacity determined by the pseudo-second-order kinetic model shows greater concordance with experimental results compared to its pseudo-first-order counterpart (Table 3). Parallel results were found in a separate study, which established that the adsorption of melamine on Fe(III) and Mn(II) ions adheres to a pseudo-second-order kinetic model (Peng et al., 2020).

Adsorption isotherms shed light on the connection between the concentration of adsorbent in the solid phase and its presence in the liquid phase under balanced conditions (Keshavarza et al., 2020). The adsorption isotherms for Fe(III) and Mn(II) ions were studied using two distinct frameworks, namely, the Langmuir isotherm and Freundlich isotherm. The linear formulations for both Langmuir and Freundlich isotherms can be articulated as follows.

$$\frac{C_e}{q_e} = \frac{C_e}{q_m} + \frac{1}{K_L q_m} \quad (4)$$

$$\log q_e = \log K_F + \left(\frac{1}{n}\right) \log C_e \quad (5)$$

The variable used in equations is as follows. The maximum adsorption capacity represented in  $q_m$  (mg/g).  $K_L$  (L/mg) is a constant on the Langmuir isotherm, while  $K_F$  is the Freundlich constant (mg/g)(mg/L). The intensity and surface heterogeneity at different concentrations is denoted by  $1/n$  (Wang et al., 2019).

Table 4 presents the adsorption parameters of Fe(III) and Mn(II) ions using the Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composite. The  $R^2$  for the Langmuir isotherm is closer to 1 than the Freundlich isotherm. This observation suggests that the adsorption process of Fe(III) and Mn(II) ions onto this composite occurs predominantly as a monolayer, consistent with the principles of Langmuir adsorption (Dai et al., 2012)

**Table 3.** The kinetics parameters for the adsorption of Fe(III) and Mn(II) ions

Adsorption kinetics	Fe(III)	Mn(II)
Pseudo-first-order		
$R^2$	0.9692	0.9731
$k_1$ (min <sup>-1</sup> )	0.0969	0.973
$q_{e \text{ (calc)}}$ (mg/g)	39.18	23.21
Pseudo-second-order		
$R^2$	0.9971	0.9948
$k_2$ (g/mg·min)	0.0031	0.0238
$q_{e \text{ (calc)}}$ (mg/g)	90.91	42.07
$e_{\text{ (eksp)}}$ (mg/g)	85.41	36.92

**Table 4.** The parameter of isotherm in the adsorption of Fe(III) and Mn(II) ions

Isotherm adsorption	Fe(III)	Mn(II)
Langmuir		
R <sup>2</sup>	0.9962	0.9951
K <sub>L</sub> (L/mg)	0.361	0.085
q <sub>m</sub> (mg/g)	322.58	208.33
Freundlich		
R <sup>2</sup>	0.9696	0.9931
K <sub>F</sub> (g/mg.min)	27.88	4.78
n	2.006	1.549

Table 5 provides a comparative evaluation of the capacity of adsorption of different adsorbents for Fe(III) and Mn(II) ions. The adsorption capacity exhibited in this research exceeds those reported in prior studies.

### The thermodynamics of the adsorption

The influence of temperature on adsorption capacity is a fundamental aspect in the study of adsorption thermodynamics. To elucidate this, a sequence of experiments was conducted at distinct temperatures, specifically 25°C, 35°C, 45°C, and 55°C. The examination incorporated key thermodynamic parameters such as Gibbs free energy ( $\Delta G^\circ$ ), enthalpy change ( $\Delta H^\circ$ ), and entropy change ( $\Delta S^\circ$ ). The computation of these parameters is achieved through specific thermodynamic equations.

$$\ln\left(\frac{q_e}{C_e}\right) = \frac{\Delta S^\circ}{R} - \frac{\Delta H^\circ}{RT} \quad (6)$$

In the equation,  $R$  stands for the universal gas constant, which has a value of 8.314 J/mol K.  $T$  denotes the absolute temperature expressed in Kelvin (K). To derive the values of  $\Delta H^\circ$  and  $\Delta S^\circ$ , a plot is created with  $\ln(q_e/C_e)$  on the y-axis and  $1/T$  on the x-axis. The slope and intercept of this plot correspond to  $\Delta H^\circ$  and  $\Delta S^\circ$  respectively. The  $\Delta G^\circ$  can then be calculated using an appropriate formula:

$$\Delta G^\circ = \Delta H^\circ - T\Delta S^\circ \quad (7)$$

The data presented in Table 6 indicates that the binding of Fe(III) and Mn(II) ions to the Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composite is an exothermic process, as evidenced by the positive  $\Delta H^\circ$  values. In contrast, the negative  $\Delta S^\circ$  values imply that these adsorption processes are not only spontaneous but also irreversible when it comes to metal adsorption. The appearance of negative  $\Delta G^\circ$  values at various temperatures indicates a tendency towards spontaneity in the adsorption process. Moreover, as temperature increases, there is a corresponding rise in  $\Delta G^\circ$  value, suggesting an increased propensity for adsorption with higher temperatures.

**Table 5.** A comparative analysis of the capacity of Fe(III) and Mn(II) ions to be absorbed into various adsorbents

Ions	Adsorbent	pH	Initial concentration (mg/L)	Time (min)	Capacity (mg/g)	Reference
Fe(III)	Chitosan	3	6	60	90.09	Ngah et al., 2005
	Hazelnut hull	3	20	70	13.59	Sheibani et al., 2012
	Zeolite NaY	5	120	30	57.80	Kulawong and Kulawong, 2018
	Brown bentonite	-	200	120	16.65	Bakalar et al., 2020
	Activated carbon from Bombax ceiba fruit shell	3.5	75	25	37.16	Brishti et al., 2023
	Fe <sub>3</sub> O <sub>4</sub> /CaO/PDA	3	400	60	322.58	In this study
Mn(II)	Chitosan/poly ethylene glycol blend membrane	6	10	80	21.7	Reiad et al., 2012
	Natural zeolite	6	25–250	240	7.68	Ates, 2014
	Carbon impregnated CTAB	7	50	420	43	Anbia et al., 2016
	Banana peels-activated carbon	4	1.351	30	-	Khairiah et al., 2021
	Blast furnace slag	5.2	30	50	59.88	Chouchane et al., 2023
	Fe <sub>3</sub> O <sub>4</sub> /CaO/PDA	5	400	60	208.33	In this study

**Table 6.** Thermodynamic parameters for the adsorption of Fe(III) and Mn(II) ions

Ions	Parameters (kJ/mol)	Temperature (°C)			
		25	35	45	55
Fe(III)	$\Delta G^\circ$	-24.956	-25.399	-25.842	-26.284
	$\Delta H^\circ$	-11.754			
	$\Delta S^\circ$	0.044			
Mn(II)	$\Delta G^\circ$	-19.498	-19.814	-20.130	-20.446
	$\Delta H^\circ$	-10.075			
	$\Delta S^\circ$	0.032			

## CONCLUSION

CaO was effectively derived from the shells of green mussels and used as a precursor for the manufacture of composites consisting of Fe<sub>3</sub>O<sub>4</sub>, CaO, and PDA. The composite of Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA shown a notable adsorption capacity for Fe(III) and Mn(II) ions, specifically measuring 322.58 mg/g and 208.33 mg/g. A further advantage of Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composite is its simple separation from the solution, which can be accomplished in a short amount of time using an external magnet, the separation procedure is more cost-effective. The results indicate that the Fe<sub>3</sub>O<sub>4</sub>/CaO/PDA composite has promising remediation potential for acid mine runoff. AMD is characterized by a heightened presence of heavy metal ions, hence requiring the adoption of a suitable resolution to address this issue.

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