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# Optimization of *Olea europaea* Stone-Activated Carbon Preparation Using Response Surface Methodology for Thiamphenicol Removal in a Fixed Bed Column

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# ABSTRACT

The study addresses the persistent issue of thiamphenicol (THI) accumulation in aquatic environments and its detrimental impact on biological systems. While activated carbon is commonly used for removing such organic micropollutants in advanced wastewater treatment, this research explores the innovative use of olive stones as a feedstock for activated carbon production. The novelty of this study lies in the optimization of the activated carbon preparation process using a fractional factorial design with five critical factors: concentration, heating rate, activation temperature, activation time, and impregnation ratio. By employing the methylene blue method to determine the specific surface area (SSA), the optimal conditions were identified: a phosphoric acid solid-liquid ratio of 1:2 (74.52%), a heating temperature of 550 °C at a rate of 10 °C/min, and an activation period of 120 minutes, resulting in an SSA of 53.07 m<sup>2</sup>/g. The subsequent THI adsorption tests in a fixed-bed column revealed that THI removal efficiency was inversely proportional to flow rate and initial THI concentration, while positively correlated with bed height. This study fills a critical gap by demonstrating an effective, sustainable method for producing activated carbon from agricultural waste, optimizing the process parameters for maximum efficiency in micropollutant removal.

**Keywords:** olive fruit stones, activated carbon, response surface methodology, thiamphenicol, adsorption, fixed bed column.

# INTRODUCTION

Even small amounts of emerging contaminants, known as micropollutants, pose major hazards to aquatic ecology. Hospital, household, and industrial activities generate them, either directly or indirectly (Mailler et al., 2017). Pharmaceutical micropollutants are the most widespread and dangerous pollutants for aquatic biota; therefore, they are considered a main emerging issue (Busch et al., 2016). Recently, a great deal of interest has been focused on the use of veterinary antibiotics (VAs), which are considered hazardous to the environment, in veterinary and human medicine. Between 17% and 90% of VAs are eliminated as the active component after being administered to animals, and they subsequently enter the environment via their faeces or urine (Carvalho and Santos, 2016). Thiamphenicol (THI) is a common antibiotic used to control bacterial illnesses and is used in aquaculture and animal husbandry (Li et al., 2014). However, the negative effects of THI, such as its hematotoxicity, embryotoxicity, and potent immunosuppressive activity, affect how well plant microbes function physiologically and in animals (Maita et al., 1999). THI may also enter surface wastewater and water through animal metabolism, wastewater discharge, and rain runoff, which readily produces toxins in humans and the environment via the food chain (Sim et al., 2011). Thus, a practical and highly effective technique is required to eliminate THI from water.

To eliminate organic contaminants from wastewater and water, activated carbon (AC) has been employed extensively (Sabio et al., 2006; Sotelo et al., 2014, 2012a). AC has several advantages, and its main features are its large surface area and simple regeneration by solar energy (Miguet et al., 2016; Suhas et al., 2016). AC has a highercapacity of absorption and can be useful in the removal of some organic pollutants. According to certain research, AC has a 100% removal efficiency. Adsorption by AC is used in column mode in practical operations (Putra et al., 2009). In terms of cost ratio and quality, chemical activation offers the best end product and has been more thoroughly investigated in previous research than physical activation (Heidarinejad et al., 2020a). An activating agent is often either a basic or an acid. Potassium hydroxide and phosphoric acid are the most effective activating agents (Azmi et al., 2015; Balogoun et al., 2015; Gueye et al., 2014; Heidarinejad et al., 2020b; Li et al., 2017). The primary factors influencing the quality of AC are the impregnation ratio, time and temperature of activation, concentration, and heating rate (Das and Mishra, 2017). These major variables could be optimised using the RSM method for preparing the AC solution (Asfaram et al., 2015; Senthilkumar et al., 2017). Research in the literature indicates that AC possesses both a high removal effectiveness and a high adsorption capacity. The removal efficiency in some applications can reach 100%. Furthermore, the USEPA Agency has recognized AC as a better technique for treating a variety of controlled organic pollutants (Sotelo et al., 2012b). The column mode is used in a number of applications and experimental studies for AC adsorption treatment (Patel et al., 2022). Column adsorption offers several benefits, including a straightforward mode of operation, effective process control, and the potential for high removal efficiencies. Moreover, the procedure may be easily expanded from the laboratory to industrial implementation.

Various biomasses, such as coconut tree waste (Freitas et al., 2019; Jawad et al., 2017), peach stones, rice husk (Álvarez-Torrellas et al., 2016), bagasse from sugarcane (Chakraborty et al., 2018), palm shell (Mustafa et al., 2022) and raw bamboo (Ismail et al., 2022), have been used for AC preparation. In this study, olive fruit stones were chosen because of their abundance in the Mediterranean region. Olive stones are well known and abundant agricultural byproducts in regions where they are widely farmed. Approximately 57% of Morocco's total tree acreage is made up of olive trees, which are the primary fruit species cultivated there (Elabdouni et al., 2020). This variety of fruit may be found all across the country since it can adapt to any bioclimatic zone in Morocco. Many studies have been conducted on the AC efficiency of common contaminants obtained from olive stone waste, including dyes (Al-Ghouti and Sweleh, 2019; Hazzaa and Hussein, 2015) as well as heavy metals (Alslaibi et al., 2013; Corral-Bobadilla et al., 2021). The adsorption of emerging pollutants, such as ketoprofen, has been studiednaproxen, diclofenac (Baccar et al., 2012), amoxicillin (Mansouri et al., 2015), and ibuprofen (Mansouri et al., 2015), using olive stone AC; the related adsorbed quantities were respectively 24.7, 39.5, 56.2, 158.83 and 178.04 mg.g<sup>-1</sup>. In this study, we investigated the adsorption capabilities of carbon derived from olive fruit stones, chemically activated with  $H_3PO_4$ , for removing THI. Our research focused on utilizing this innovative adsorbent, derived from agricultural waste, for effective THI removal.

### MATERIALS AND METHODS

#### Preparation of feedstock

Olive fruit stones (*Olea europaea*) from the Errachidia province of Morocco were used as precursor material. This material was collected, previously washed in water, and then dried. The following step consists of crushing the olive stones into smaller fragments by mechanical grinding. Then, we sieved them to obtain particles with sizes between 400  $\mu$ m < G < 640  $\mu$ m. The grains were repeatedly rinsed with hot distilled water until aroma disappeared and rinse water was clear. They were then oven-dried for 24 hrs at 110 °C.

### Activated carbon preparation of and statistical experimental design approach

Approximately 20 g of sample was inserted into a covered crucible and then heated at 400 °C by a muffle furnacefor an hour with 5 °C per minute as rate in an anoxic environment. This was how the carbonization procedure was carried out. After cooling, the samples were cooled to room temperature. In this work, a statistical experimental design was used with JMP<sup>11</sup> software to define variables for activation. To optimize these processes, the surface of RSM, a statistical and mathematical set of techniques, is adequate. The goal is to maximize the reaction, which is affected by a number of variables (Baş and Boyacı, 2007). The RSM model is a whole quadratic Equation 1 or a shortened version of it. The following equation represents the second-order model:

$$Y = \beta_0 + \sum_{j=1}^{\kappa} \beta_j X_j + \sum_{j=1}^{\kappa} \beta_{jj} X_j^2 + \sum_{i < j} \beta_{ij} X_i X_j \quad (1)$$

In this Equation, Y represents the anticipated response,  $\beta_0$  denotes the coefficient intercept,  $\beta_i$ ,  $\beta_{ij}$ ,  $\beta_{ij}$  signifies respectively the linear, the squared and interaction terms, as well as  $X_i$  and  $X_j$  are coded as independent variables.

With the fewest number of tests, the CCD design and RSM model may be used to adjust the surface to maximize the important factors and explore the relationships and interplay between the parameters (Hameed et al., 2008).

The AC by phosphoric acid (ACPA) depends on several parameters. To determine the ideal efficiency settings for each variable that guarantees a high specific surface area (SSA "Y") computed using the methylene blue technique. The methylene blue (MB) value is considered to have the greatest response when AC is being prepared (Itodo et al., 2010). The MB approach was employed to determine the surface area that was accessible to relatively large molecules in the sample. Twenty-five millilitres of the solution of methylene blue was taken at various concentrations, and 0.1 g of the sample was mixed for two hours before being centrifuged and tested. Equation 2 can be applied to calculate the surface area using Langmuir's isotherm (Azoulay et al., 2020).

$$SSA = \frac{b \times N \times S}{M} \tag{2}$$

where: *SSA* is the surface area  $(m^2g^{-1})$ ; *b* is the maximal capacity of adsorption (mg/g) obtained from the isotherm of Langmuir; *N* stand to the Avogadro number, *M* hydrated MB molar mass (319.86 g/mol); and *S* is the surface area covered by methylene blue molecules (119 Å<sup>2</sup>). A two-level and five-factor central composite design (CCD) (weight % of phosphoric acid (wt% PhA), solid–liquid ratio, temperature, heating rate, and activation time) was used in our study as the experimental design (Baccar

et al., 2012; García-Mateos et al., 2015; Mansouri et al., 2015; Sun et al., 2012).

These important parameters will have an impact on the resulting AC properties. Table 1 indicate the independent variables' as well as their coded levels. To facilitate the regression, the variables' values were coded, with + 1 denoting the highest level and -1 denoting the lowest level.

The fractional factorial design experiment  $2^{k-r}$  was completed by a start design experiment  $2 \times k$  and replicated center experimental point N<sub>0</sub> (the number of center points in this study is 3) with K = the number of variables; in our study, we have five variables and r = the fraction of the full factorial, which is equal to 1. Thus, the required experiments number (N) is determined by N =  $2^{k-r} + 2k + N_0$  (Bencheikh et al., 2021; Bhattacharya, 2021; Tarley et al., 2009).

The output data were statistically evaluated using variance analysis (ANOVA). In addition, we aimed to determine the best conditions for carbon activation as well as the significance and impact of factors both independent and interacting in the modelling.

# Characterization of the optimized activated carbon by phosphoric acid (OACPA)

Many methods have been adopted to analyse AC samples, in particular XRD, FTIR and  $N_2$  adsorption–desorption isotherm analysis (Quantachrome Touchwin<sup>TM</sup> v1. 22). These techniques are required to provide information on the characteristics of such synthesized AC, which is helpful for further understanding.

Spectral characterization: Using a KBr disc and a burka-tensor 27 spectrometer in reflection mode, the FT-IR spectrum of the optimal AC was recorded between 400 cm<sup>-1</sup> and 4000 cm<sup>-1</sup>.

X-ray powder diffraction (XRD) analysis was employed to investigate the phase/crystallographic composition of the optimum AC.

#### Adsorbate preparation

Adsorption was carried out on thiamphenicol's active ingredient (97.5% purity. Each chemical used in this study is of the analytical class. A stock solution of 100 mg $\cdot$ L<sup>-1</sup> was obtained by dissolving thiamphenicol (100 mg) in 1 liter of distilled water in a 1 liter measuring flask. The THI of the solution was detectable at a wavelength of

Parameter	Levels						
Variables	Symbols	-α	-1	0	+1	+α	
Phosphoric acid weight %	X <sub>1</sub>	29.52	40	57.26	85	85	
Activation time (min)	X <sub>2</sub>	41.78	60	90	120	138.22	
Solid–Liquid (ratio)	X <sub>3</sub>	0.17	0.25	0.38	0.5	0.58	
Heating rate (°C.min <sup>-1</sup> )	X <sub>4</sub>	8.48	10	12.5	15	16.52	
Temperature (°C)	X <sub>5</sub>	419.64	450	500	550	580.36	

Table 1. Variables with coded levels according to the central composite design

225 nm, and all studied solutions were measured with a Shimadzu UV-1900i spectrophotometer.

adsorption efficacy of optimal AC by phosphoric acidwith a height of 1cm and 1 ml.min<sup>-1</sup>as rate.

#### Studies in stationary bed columns

#### Experimental process

The use of mini-columns in the study of adsorption dynamics constitutes a simple method (Rosene et al., 1976). In this work, the adsorbent was placed in a column (1.4 cm in diameter), where process of adsorption took place. The rate of the adsorbate passes into the column. To guarantee that the materials inside the column were secure, a layer of support cotton was placed on the bottom of the column. First, cotton was placed for prevention the adsorbent from sliding off the column; the necessary amount of AC was then added to the column. The second layer of cotton was positioned on top of the adsorbent bed to guarantee that the adsorbent within the column was unable to move. The effects of bed height, starting THI concentration, and THI flow rate were the three main factors of this investigation. A peristaltic pump managed the volume of fluid in the fixed-bed column at any given time. The desired sample solution was continuously collected at the exit as the solution flowed into the column. A UV spectrophotometer was employed to measure the treated water concentration. All findings from this study, carried out at a pH of 5.7 and in 24 °C, were used to analyse the breakthrough curve.

#### Flow rate effect

The effects of various rates (1 mL/min and 4 mL/min) on THI adsorption by the optimal AC of phosphoric acid were investigated. The concentration of THI as well as adsorbent bed height were initially maintained at 15 mg $\cdot$ L<sup>-1</sup> and 1 cm.

#### Initial THI concentration effect

Initial concentrations of THI (5.5 mg·L<sup>-1</sup>, 15 mg·L<sup>-1</sup>) were investigated for their effect on the

Bed-depth effect

The optimal AC effect of phosphoric acid on the THI was examined at 1 cm, 1.7 cmofbedheights. THI was added at a fixed starting concentration (15 mg·L<sup>-1</sup>) with 1 mL·min<sup>-1</sup> asrate.

#### Adsorption column performance

The performance and reactivity of a column are highly influenced by the onset time and the break-through curve form. Operating properties, in particular the throughput rate, initial adsorbate concentration and bed height, have a significant impact on the experimental determination of these parameters. The breakthrough curve, which is typically represented by  $C_t/C_0$  versus time (Delgado et al., 2022), illustrates how a drug is loaded into a fixed bed to be removed from the solution. Equations 3, 4, 5 and 6 of the effluent volume  $(V_{eff})$ , the total quantity of adsorbate adsorbed  $(q_{total})$ , the amount applied to the column  $(m_{total})$ , and the total adsorbate removal percentage (%R) (Cruz-Olivares et al., 2013; Kavianinia et al., 2012) are calculated as follows:

$$V_{eff} = Qt_{total} \tag{3}$$

$$q_{total} = \frac{Q}{1000} \int_{t=0}^{t=t} Cads \, dt \tag{4}$$

$$m_{total} = \frac{QC_0 t_{total}}{1000} \tag{5}$$

$$\% R = \frac{q_{total}}{m_{total}} \times 100 \tag{6}$$

where:  $t_{total}$  represents the overall duration of fluid flow through the column (in minutes); Qstands for the solution volume at a particular instant (in mL/min);  $q_{total}$  is the total adsorbate adsorbed in mg/g, where the adsorbed pollutant concentration is calculated by  $Cads = (C_0 - C_e)$ ;  $C_e$  (mg/g) as well as  $C_0$  (mg.L<sup>-1</sup>) are the effluent and influent pollutant concentrations; and  $m_{total}$  is the total adsorbate applied to the column in mg.

# **RESULTS AND DISCUSSION**

# Experimental design for optimizing activated carbon preparation

The experimental design was applied using JMP<sup>11</sup> software, and central composite design (CCD) was used to correlate the specific surface area (SSA ( $m^2/g$ )) calculated by the methylene blue value (Y) with the phosphoric acid weight % (X<sub>1</sub>),

solid – liquid ratio  $(X_2)$ , temperature  $(X_3)$ , heating rate  $(X_4)$ , and activation time  $(X_5)$ . The most important feature of AC in the adsorption process is its specific surface area. The number of experiments required N = 25 - 1 + 2 × 5 + 3 = 29 is the total number of tests required for the experiments required for statistical modelling. The experimental design data set and the response values noted in the experimental outcomes are shown in Table 2.

#### Variance analysis

Analysis of variance is a crucial statistical technique for evaluating the validity of a model.

	F		2	,							
							Actu	al parame	eters		Response
		(		vei		X <sub>1</sub>	X <sub>2</sub>	X <sub>3</sub>	X <sub>4</sub>	X <sub>5</sub>	Y
Run	X <sub>1</sub>	X <sub>2</sub>	X <sub>3</sub>	X <sub>4</sub>	X <sub>5</sub>	Phosphoric acid weight %	Activation time (min)	Solid– Liquid (ratio)	Heating rate (°C/ min)	Temperature (°C)	SSA (m²/g)
1	-1.61	0	0	0	0	29.52	90	0.375	12.5	500	0.92
2	-1	-1	-1	-1	-1	40	60	0.25	10	450	9.09
3	-1	-1	-1	1	1	40	60	0.25	15	550	5.97
4	-1	-1	1	-1	1	40	60	0.5	10	550	9.10
5	-1	-1	1	1	-1	40	60	0.5	15	450	6.86
6	-1	1	-1	-1	1	40	120	0.25	10	550	6.79
7	-1	1	-1	1	-1	40	120	0.25	15	450	9.86
8	-1	1	1	-1	-1	40	120	0.5	10	450	4.94
9	-1	1	1	1	1	40	120	0.5	15	550	27.43
10	0	-1.61	0	0	0	57.26	41.78	0.38	12.5	500	7.30
11	0	0	-1.61	0	0	57.26	90	0.17	12.5	500	8.53
12	0	0	0	-1.61	0	57.26	90	0.38	8.48	500	11.29
13	0	0	0	0	-1.61	57.26	90	0.38	12.5	419.64	8.36
14	0	0	0	0	0	57.26	90	0.38	12.5	500	9.29
15	0	0	0	0	0	57.26	90	0.38	12.5	500	9.99
16	0	0	0	0	0	57.26	90	0.38	12.5	500	8.92
17	0	0	0	0	1.61	57.26	90	0.38	12.5	580.36	10.74
18	0	0	0	1.61	0	57.26	90	0.38	16.52	500	9.51
19	0	0	1.61	0	0	57.26	90	0.58	12.5	500	4.39
20	0	1.61	0	0	0	57.26	138.22	0.38	12.5	500	5.17
21	1	-1	-1	-1	1	74.52	60	0.25	10	550	19.63
22	1	-1	-1	1	-1	74.52	60	0.25	15	450	7.96
23	1	-1	1	-1	-1	74.52	60	0.5	10	450	8.49
24	1	-1	1	1	1	74.52	60	0.5	15	550	7.06
25	1	1	-1	-1	-1	74.52	120	0.25	10	450	0.99
26	1	1	-1	1	1	74.52	120	0.25	15	550	8.72
27	1	1	1	-1	1	74.52	120	0.5	10	550	57.23
28	1	1	1	1	-1	74.52	120	0.5	15	450	5.68
29	1.61	0	0	0	0	85	90	0.38	12.5	500	8.98

Table 2. Experimental design results of the ACs studied

When the response variable is influenced by random variations, the model's variance is assessed using the regression mean square. For a robust model, the regression mean square and the ratio of the residual mean square should ideally converge to unity, indicating a good fit (Bouiti et al., 2024).

In this study, a 95% confidence level was set as the threshold for statistical significance. The primary aim was to determine whether the proposed model could accurately capture the inherent variability within the data. By examining both inter-group and intra-group variations, ANOVA provides the necessary analytical framework to achieve this objective.

In this research, an analysis of variance was carried out to establish the statistical significance of the proposed models (Samghouli et al., 2022) for the specific surface area (Y) and the independent variables ( $X_1$ ,  $X_2$ ,  $X_3$ ,  $X_4$ , and  $X_5$ ). The results acquired from the variance analysis of the specific surface area of the carbon activated by phosphoric acid are shown in the Table 3.

Table 3 presents the results of variance analysis for the response's coded modelling. The data show that the proposed model for the SSA of activated carbon by phosphoric acid (Y) is statistically significant at the 5% confidence level (p values  $\leq$ 0.05) (Azoulay et al., 2020; dos Reis et al., 2016) and that SSA (p value = 0.04) has a p-value inferior to 0.05. The correlation coefficient of the AC specific surface area studied is 0.89 (Figure 1a), and the  $RSq_{Adj}$  is 0.64, which probably indicates the compatibility between the data and the model. The SSA of the AC residue from each experiment is shown in Fig. 1b. Therefore, the residue graph shows a reasonable spatial distribution, proving that the model adequately describes this study.

# Estimated parameters and mathematical model

Analysis of the pvalues for the interplay between time and solid–liquidratio, the interplay between phosphoric acid weight and heating rate, the temperature, the interplay between time and temperature, and the interplay between solid/liquidratio and temperature showed that those variables were probably statistically significant for the specific surface area, with p values of 0.01, 0.01, 0.01, 0.02, and 0.04, respectively. The p-values of remaining factors were greater than 0.05, which indicates statistically insignificant. (Di Leo and Sardanelli, 2020; dos Reis et al., 2016).

Based on Table 4's results, the complexity of the regression analysis model was minimized by eliminating all no significant components, and the best fit of the second-order polynomial model equations is given by Equation 7. This equation describes the SSA of the AC by phosphoric acid, and the signs positive and negative before each

 Table 3. Analysis of variance for the quadratic polynomial surface response modelling of carbon activation by phosphoric acid

Source	DF	Sum of squares	Mean square	F Ratio
Model	20	2655.77	132.79	3.49
Error	8	303.82	37.98	P value
Total corrected	28	2959.59		0.04*



Figure 1. (a) Experimental predicted response and (b) analysis of the residual of the specific surface area SSA of AC

Term	Estimate	Std Error	t Ratio	P value
Model	6.62	2.76	2.40	0.04*
X <sub>1</sub> (Wt%PhA)	2.30	1.34	1.72	0.12
X <sub>2</sub> (time)	2.08	1.34	1.55	0.15
X <sub>3</sub> (Solid–Liquid (ratio))	2.41	1.34	1.80	0.11
X <sub>4</sub> (Heating rate)	-1.86	1.34	-1.40	0.20
X <sub>5</sub> (Temperature)	4.34	1.34	3.24	0.01*
X <sub>1</sub> · X <sub>2</sub> (Wt%PhA*time)	0.71	1.54	0.47	0.65
X <sub>1</sub> · X <sub>3</sub> (Wt%PhA · Solid–Liquid (ratio))	1.53	1.54	1.00	0.35
$X_2 \cdot X_3$ (time · Solid–Liquid (ratio))	5.01	1.54	3.25	0.01*
$X_1 \cdot X_4$ (Wt%PhA · Heating rate)	-4.82	1.54	-3.13	0.01*
$X_2 \cdot X_4$ (time · Heating rate)	0.01	1.54	0.01	0.99
$X_3 \cdot X_4$ (Solid–Liquid (ratio) · Heating rate)	-1.80	1.54	-1.17	0.27
$X_1 \cdot X_5$ (Wt%PhA · Temperature)	3.19	1.54	2.07	0.07
$X_2 \cdot X_5$ (time (min) · Temperature)	4.34	1.54	2.81	0.02*
$X_{_3} \cdot X_{_5}$ (Solid–Liquid (ratio) · Temperature)	3.85	1.54	2.50	0.03*
$X_4 \cdot X_5$ (Heating rate $\cdot$ Temperature)	-3.15	1.54	-2.04	0.07
$X_1 \cdot X_1$ (Wt%PhA · Wt%PhA)	0.02	1.66	0.01	0.99
$X_2 \cdot X_2$ (time $\cdot$ time)	0.52	1.66	0.31	0.76
$X_3 \cdot X_3$ (Solid–Liquid (ratio) · Solid–Liquid (ratio))	0.60	1.66	0.36	0.73
$X_4 \cdot X_4$ (Heating rate $\cdot$ Heating rate)	2.13	1.66	1.28	0.23
$X_5 \cdot X_5$ (Temperature $\cdot$ Temperature)	1.79	1.66	1.08	0.31

**Table 4.** Estimated effects for the model of the quadratic polynomial of SSA (\*indicates that the correlation term is statistically significant)

factor's coefficient correspond to the synergic and antagonistic effects, respectively.

$$Y = 6.62 + 5.01X_{2}X_{3} - 4.82X_{1}X_{4} + 4.34X_{5} + 4.34X_{2}X_{5} + 3.85X_{3}X_{5}$$
(7)

#### Parameter optimization of the OACPA

The statistical approach helps in predicting the specific surface area max potential at the optimum level of the variables that are independent. We will determine the optimum conditions for maximum yield while minimising variability. According to Fig. 2, the maximum SSA of AC that may be achieved under optimal conditions is 65.27 m<sup>2</sup>/g. The optimal conditions for obtaining the highest SSA of OACPA are reported in Table 5.

The 3D response surface plot (Fig 3.b) demonstrates that the effect of two independent

factors (significant variables obtained in the model equation) on the specific surface area changes simultaneously. The AC of phosphoric acid (Fig. 3.b1) shows inter actions between the ratio of solid to liquid and the activation temperature, and the maximum specific surface area values correspond to the highest temperatures and biochar-H<sub>2</sub>PO<sub>4</sub>ratio. For the interplay between the solid-liquid ratio and time, the best specific surface area results were obtained with a longer activation time and a greater ratio of biochar-H<sub>2</sub>PO<sub>4</sub> (Fig. 3. b2). Figure 3. b3 indicates the interplay between the activation temperature and time; the specific surface increases as both factors increase. On the other hand, the interplay between the phosphoric acid weight % and the heating rate showed that the SSA increased when the phosphoric acid weight % increased and the heating rate decreased (Fig 3. b4).

Table 5. Optimal conditions for obtaining a high specific surface area for RSM and validating the experimental results

Setting	Wt% PhA	Time (min)	Solid–liquid (ratio)	Heating rate (°C/min)	Temperature (°C)	SSA (m²/g)	SSA (m²/g) Lower	SSA (m²/g) Upper	Desirability
Optimal condition	74.52	120	0.5	10	550	53.07	39.46	66.69	0.53



Figure 2. Prediction profiler showcasing the models and settings that contributes to achieving maximum overall desirability



**Figure 3.** (b) Effect of independent variables in the three-dimensional response surface on the external surface area, (b1) effect of solid – liquidratio (0.25; 0.5) and temperature (450 °C; 550 °C), (b2) effect of time (60 min; 120 min) and solid–liquidratio (0.25; 0.5), (b3) effect of temperature (450 °C; 550 °C) and time (60 min; 120 min) and (b4) heating rate effect (10 °C.min<sup>-1</sup>;15 °C.min<sup>-1</sup>) as well as Wt% of phosphoric acid (40%; 85%)

#### **Characterization of OACPA**

#### X-ray diffraction analysis

The diffractogram (Fig. 4) of the raw olive fruit stones shows that, in general, their structure is amorphous, and the peak at  $2\Theta = 22.5$  corresponds to the cellulose structure (Kaya et al., 2018; Seydibeyoğlu et al., 2017).

The peak at approximately  $2\theta = 22^{\circ} - 25^{\circ}$  of OACPA was indexed as C (002) diffraction, revealing the amorphous structure of carbon with randomly oriented aromatic rings. The peak present at  $2\theta = 42^{\circ}$ -  $45^{\circ}$  is related to the structure of C (100) graphite (Dehkhoda et al., 2014; Hu et al., 2014; Jamil et al., 2020).

#### FTIR analysis

The main peaks that appear in the spectrum of the raw olive fruit stone (Fig. 5) are attributed to lignin, cellulose, and hemicelluloses in the lignocelluloses' compounds. This result is similar to that obtained for the lignocelluloses' groups in other studies (Baccar et al., 2009). The band placed at 3304.23 cm<sup>-1</sup> correspond to the vibrations O-H in the hydroxyl, phenol, as well as acid grps (Xu et al., 2013). Moreover, the high peaks at 2922 cm<sup>-1</sup> as well as 2856 cm<sup>-1</sup> are ascribed to C-H vibration stretching in alkyl groups. According to Xu et al. (Xu et al., 2013), these distinctive peaks represent lignin and hemicelluloses, respectively. At 1748 cm<sup>-1</sup>, the carbonyl group C = O peak may be observed (Roğlu et al., 2017). The alkene group (C = C) vibrations are visible at approximately 1641.11 cm<sup>-1</sup>, but the aromatic ring C = C vibrations are visible at approximately 1506.92 cm<sup>-1</sup>. Alkyl and hydroxyl groups, which are the basic building blocks of lignocelluloses' groups, are responsible for the peaks at 1466 cm<sup>-1</sup> as well as 1386 cm<sup>-1</sup> (Baccar et al., 2009). The band at 1316 cm<sup>-1</sup> could be corresponded to the vibrations C–O of carboxylate grps. The peak at 1254 cm<sup>-1</sup> can be the result of phenol groups, ethers, or esters (Durán-Valle et al., 2005). The peaks corresponding to C-O stretching are located between 1160–1042 cm<sup>-1</sup> (Baccar et al., 2009).

The FTIR spectrum of OACPA shows a few peaks that are comparable to those of raw olive fruit stones, verifying that the effect of phosphoric acid treatment was caused by significant chemical modifications. Considering the OACPA spectrum, the peak at 1039 cm<sup>-1</sup> for OACPA decreased in intensity compared with that of the spectrum of the raw olive fruit stones. According to Jiang et al. (Jiang et al., 2012), this peak is assigned to P-O, indicating the reaction of H<sub>2</sub>PO, with OACPA. It is hypothesized that phosphoric acid added oxygenated functional groups to the biochar, which is predicted to have significant effects on the performance of OACPA as an adsorbent. One possible explanation for the broad peak at 1163 cm<sup>-1</sup> is the asymmetric stretching of O-P-O (Jiang et al., 2012). According to Benaddi et al., dehydrating cellulose using H<sub>3</sub>PO<sub>4</sub> acid similarly to dehydrating



Figure 4. XRD patterns of the raw olive fruit stones and OACPA

alcohols. Moreover, they proposed that phosphorous oxides exhibit Lewis acid behaviour and could form the bonds C-O-P at elevated temperatures (Benaddi et al., 1998). The absence of peaks between 1254–1506.92 cm<sup>-1</sup> was noted, except for the peak at 1316 cm<sup>-1</sup>, which exhibited a reduction in intensity. Similar findings were reported in Benzekri et al., who suggested that this particular peak may arise from the asymmetric bending vibration of the -CH, group (Benzekri et al., 2018). The band at 1567.8  $cm^{-1}$  corresponds to C = C in aromatic groups. This indicates that the amount of aromatic groups present in the structure of OACPA increased. A peak at 1641.11 cm<sup>-1</sup> corresponding to alkene groups completely disappeared. A sharp reduction in the band intensity at 1748 cm<sup>-1</sup> represents C = O groups. This implies that there are fewer C = O groups in OAC-PA than in the raw olive fruit stones. The impact of  $H_2PO_4$  may be responsible for the decomposition of



Figure 5. FTIR spectrum of raw olive stones as well as OACPA

carbonyl groups and, subsequently, the decrease in the quantity of carbonyl groups. The disappearance of the peaks at 2922 cm<sup>-1</sup>as well as 2856 cm<sup>-1</sup>, which attributed to alkyl groups, and a clear decrease in the peak at 3304.23 cm<sup>-1</sup> are observed; these results are similar to those of Song et al. (Song et al., 2011).

#### Adsorption/desorption isotherms

The N<sub>2</sub> isotherms of OACPA and OFs are shown in Fig. 6. The SSA and total pore volume of the samples are given in the Table 6. The surface areas of the raw olive fruit stones and OAC-PA were 2.83 and 178.73 m<sup>2</sup>/g, respectively. The surface area of OACPA was 63 times greater than that of the raw olive fruit stones. The total pore volumes of the raw olive fruit stones and OACPA were 0.0016 and 0.1035 cm<sup>3</sup>·g<sup>-1</sup>.

#### Adsorption column performance

# Flow rate effect

The impact of the solution flow rates (1 mL/ min and 4 mL/min) on the adsorption of THI by OACPA was investigated. The THI concentration and bed height of the adsorbent respectively were held constant (1 cm and 15 mg/L). The curves shown for the adsorbate flow rates in the column under study are displayed in Fig. 7. At the lowest rate (1 mL/min), the slowest progression curve, which shows how long it took to reach equilibrium, was produced. The low THI solution flow rate allowed the molecules of adsorbate more time for diffusion, increasing the quantity of THI adsorbed throughout the column. The saturation time required to accomplish



Figure 6. N<sub>2</sub> isotherms of raw olive fruit stones and OAPAC

Samples	SSA (m²/g)	Total pore volume (cm <sup>3</sup> /g)	
Olive fruit stones	2.83	0.0016	
OACPA	178.73	0.1035	

**Table 6.** BET results of the samples



Figure 7. Breakthrough curves at different flow rates

breakthroughs drastically decreased at a THI rate of 4 mL·min<sup>-1</sup>. The total volume increases with increasing flow rate, as shown in Table 7. The total absorbance  $(q_{total})$  of AC at 1 and 4 mL/min was low at 0.41 and 0.036 mg, respectively, although that of the bed was not high. This resulted from the quick contact between THI and the adsorbent, which was caused by the fast adsorbate flow rate across the column. Due to the shorter adsorbent residence time in the column and as previously mentioned, the THI decreased from 23.56% to 2% as the THI flow rate increased from 1 to 4 mL/minute.

# Bed high effect

Figure 8 displays the breakthrough curve plots for THI uptake to study the effect of bed height (1 cm and 1.7 cm). A THI (15 mg·L<sup>-1</sup>), a flow rate (1 mL·min<sup>-1</sup>), and bed heights (1 cm and 1.7 cm) were maintained as the operational parameters. The findings indicated a potential decrease in the breakthrough curve as the bed-height improved. The parameters for the breakthrough curve at varying bed heights are presented in Table 8. Furthermore, the breakthrough curves exhibited a decline with higher adsorbent concentrations in the bed, consequently extending the overall adsorption period from 116 to 140 minutes. This alteration occurred during the adsorption process because there were more active sites available on the adsorbent surface (Iheanacho et al., 2021).

Given that more adsorbent was present, a greater amount of bed took longer to reach saturation (Fallah and Taghizadeh, 2020). In addition, compared to when a shorter bed height was employed, an increase in the mass transfer zone could be observed, slowing the progress towards equilibrium when there is no longer any mass transfer. A larger removal percentage was shown in the column because a greater bed height resulted in a greater amount of THI being eliminated. These results align with the conclusions presented in previous studies (González-López et al., 2020; Topare and Bokil, 2021).

 Table 7. Breakthrough curve parameters of the studied flow rates

Flowrate (mL/min)	t <sub>total</sub> (min)	V <sub>eff</sub> (mL)	q <sub>total</sub> (mg)	m <sub>total</sub> (mg)	% Removal
1	116	116	0.41	1.74	23.56
4	30	120	0.036	1.8	2



Figure 8. Curves obtained at various bed-heights

Table 8. Breakthrough curve parameters of the studied bed height

Bed height (cm)	t <sub>total</sub> (min)	$V_{_{eff}}(mL)$	q <sub>total</sub> (mg)	m <sub>total</sub> (mg)	% Removal
1	116	116	0.41	1.74	23.56
1.7	140	140	0.59	2.1	28.10

#### Initial concentration effect

In the column investigation, the THI adsorption is significantly impacted by the starting concentration. The THI concentration ranged between 5.5 mg/L and 15 mg/L, the remaining operational parameters remained steady, with 1 cm in bed-height and 1 mL·min<sup>-1</sup> as flow rate. Figure 9 illustrates the curves depicting the impact of initial THI concentration. Breakthrough curves were associated with higher initial concentrations, which became slower as the initial concentration decreased. Table 9 indicates that as the initial THI increases, the effluent volume decreases from 150 mL to 116 mL. A shorter period was required to reach equilibrium for the elimination of THI at higher concentrations. From breakthrough curve 7 and Table 9, we conclude that the active sites on the adsorbent surface slowly filled at lower initial concentrations. The pores on the adsorbent rapidly filled at higher initial concentrations because at higher concentrations, large amounts of THI molecules were present. A low exhaustion time was achieved at greater concentrations because the adsorbent pores were filled with THI molecules over time.



Figure 9. Breakthrough curves at different initial THI concentrations

Initial THI concentration (mg/L)	t <sub>total</sub> (min)	V <sub>eff</sub> (mL)	q <sub>total</sub> (mg)	m <sub>total</sub> (mg)	% Removal
5.5	150	150	0.43	0.83	51.81
15	116	116	0.41	1.74	23.56

Table 9. Breakthrough curve parameters of the studied bed high

# CONCLUSION

Olive stone residues can be converted into activated carbons with specific textural properties. The resulting biomaterial exhibits exceptional characteristics, making it suitable for use in fixedbed columns to remove micropollutants from water. Using OACPA, the maximum adsorption rate for THI reached 51.81%. These findings highlight the potential application of these materials in wastewater treatment processes.

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